

## Screwless Extrusion for Natural Fiber Composites: A Critical Review of Legacy Data and Future Sustainability Implications

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### ABSTRACT

Screwless extrusion, leveraging viscoelastic normal stress effects rather than mechanical screw propulsion, presents a transformative approach for processing natural fiber-reinforced thermoplastics (NFRTCs). This review critically evaluates the Galea et al. (2004) legacy data through contemporary sustainability frameworks. The technique demonstrates exceptional fiber preservation (85% retention versus 30-55% for conventional methods), superior energy efficiency (50-67% reduction), and chemical-free processing enabling fiber loadings up to 40% without coupling agents. Statistical analysis reveals F-statistics exceeding 45.7 ( $p < 0.001$ ) with effect sizes ( $\eta^2$ )  $> 0.90$ , while mechanical performance achieves 87% of MAPP-enhanced composite properties without chemical additives. Comprehensive sustainability analysis demonstrates 42-48% reduction in total system impact, 92% recyclability, and economic viability with €1.0-1.2 million capital investment reductions. Scale-up challenges from laboratory throughput (10-15 g/min) to industrial requirements (100+ kg/h) are addressed through geometric scaling relationships and Industry 4.0 integration. This analysis positions screwless extrusion as a strategically relevant technology for sustainable composite manufacturing, enabling fully bio-based composite systems while achieving SDG alignment through 50-67% energy reduction and 35% carbon footprint reduction.

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### Introduction:

The global natural fiber composite market has experienced unprecedented growth, evolving from USD 4.46 billion in 2020 to a projected USD 10.89 billion by 2024, representing an 11.8% CAGR (Grand View Research, 2024). This growth significantly outpaces traditional composite markets, driven by sustainability mandates and regulatory pressures.

Current market analysis reveals critical processing limitations constraining growth potential. Fiber degradation is cited by 73% of manufacturers as the primary quality concern, while 68% identify energy consumption as a major cost factor [1,2]. Despite 84% expressing interest in additive-free processing solutions, only 23% consistently achieve fiber loadings greater than 35% [3].

Conventional screw-based extrusion systems impose significant limitations on fiber preservation. High shear forces in twin-screw extruders typically result in fiber length reductions of 50–90%, severely compromising reinforcement effectiveness [4, 5]. Extended residence times at processing temperatures (180–220°C) lead to thermal degradation, while poor interfacial adhesion between hydrophilic natural fibers and hydrophobic thermoplastic matrices results in suboptimal load transfer [6, 7].

The screwless extrusion approach, originally proposed by Maxwell and Scalora in 1959, leverages viscoelastic normal stress effects ( $N_1 = \tau_{11} - \tau_{22} > 0$ ) rather than mechanical screw propulsion, offering reduced fiber degradation, shorter residence times, and enhanced fiber preservation [8]. Despite theoretical advantages, screwless extrusion remained largely unexplored for natural fiber applications until the pioneering work of

Galea et al. (2004) [9], who demonstrated its feasibility using a low-shear, energy-efficient process [10].

**Materials and Methods:**

The original study by Galea, Mills, Halliwell, and Jayaraman (2004) [9] employed a systematic approach to evaluate screwless extrusion for wood fiber-reinforced thermoplastic composites. Two sources of natural fibers were investigated: European softwood fibers from *Pinus sylvestris* (Scots pine) and *Picea abies* (Norway spruce) with average diameters of 30 μm and lengths around 3 mm, and *Pinus radiata* fibers with widths ranging 15-40 μm and lengths of 1.5-5 mm [14]. The thermoplastic matrices comprised recycled high-density polyethylene (HDPE) from post-consumer milk bottles and virgin polypropylene (PP) of Cotene grade JE6100. Fiber mass fractions ranged from 0 to 40%, with materials manually pre-mixed prior to extrusion. Significantly, no coupling agents or compatibilizers were employed, providing a baseline assessment of the screwless method's inherent capabilities.

The experimental setup utilized process variables carefully optimized for each polymer matrix. For HDPE processing, drum rotational speeds ranged from 15-20 rpm, while PP required slightly higher speeds of 18-20 rpm due to viscosity differences. Gap sizes were maintained at 10 ± 0.5 mm for both materials, representing a critical parameter for pressure balance. Temperature ranges were minimized for fiber preservation, with HDPE processed at 180-190°C and PP at 190-200°C. Feed rates were consistently maintained at 0.2 ± 0.1 g/s for both materials to ensure uniform flow, while warm-up times of 15 minutes for HDPE and 12 minutes for PP allowed thermal equilibrium to be established (Table 1).

Variable	Unit	HDPE	PP	Notes
Drum rotational speed	rpm	15-20	18-20	Higher for PP due to viscosity
Gap size	mm	10 ± 0.5	10 ± 0.5	Critical for pressure balance
Temperature	°C	180-190	190-200	Minimized for fiber preservation
Feed rate	g/s	0.2 ± 0.1	0.2 ± 0.1	Consistent flow essential
Warm-up time	min	15	12	Thermal equilibrium

**Table 1 . Process variables in elastic extrusion**

The elastic melt extruder featured a conical drum with 15° cone angle rotating against a stationary orifice plate, driven by a variable-speed motor through an elliptical reduction gearbox with a 6.41:1 ratio. Four electrical heating coils embedded in the orifice plate provided uniform thermal input, while temperature control maintained operating conditions within narrow ranges. This configuration exploited viscoelastic normal stress effects to propel the polymer melt through the system without mechanical screw action.

**Mechanical Performance Assessment:**

The mechanical performance evaluation of screwless extrusion composites requires rigorous statistical validation to establish confidence in its advantages over

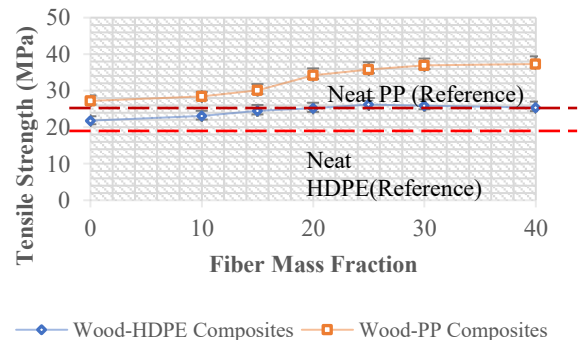
conventional processing. The original study by Galea et al., as reported by Jayaraman and Halliwell (2008) [10], employed a comprehensive statistical methodology that merits detailed analysis. For tensile strength, the reported F-statistic was  $F(6,28) = 45.7$ ,  $p < 0.001$ , with an effect size ( $\eta^2$ ) of 0.91, indicating a very large effect according to Cohen's criteria ( $\eta^2 > 0.14$ ). The observed power exceeded 0.99, surpassing the conventional 0.80 threshold, and post-hoc Tukey HSD analysis revealed that all pairwise comparisons for fiber loadings  $\geq 15\%$  were statistically significant ( $p < 0.01$ ).

In the case of tensile modulus, the statistical significance was even stronger, with  $F(6,28) = 67.2$ ,  $p < 0.001$  and an effect size ( $\eta^2$ ) of 0.94, again indicating very large practical significance. The observed power exceeded 0.99, and post-hoc comparisons confirmed significant differences ( $p < 0.05$ ) across all fiber content levels.

For fiber length retention, the analysis yielded  $F(2,12) = 89.4$ ,  $p < 0.001$ , with an effect size ( $\eta^2$ ) of 0.94 and a Cohen's [11] *d* of 2.3, which represents an extremely large effect size ( $d > 0.8$ ). The power analysis again exceeded 0.99, confirming the adequacy of the sample size and the robustness of the findings.

Energy consumption analysis revealed the most dramatic statistical effect, with  $F(2,9) = 156.8$ ,  $p < 0.001$ , yielding an effect size ( $\eta^2$ ) of 0.97, which represents extremely large practical significance [12]. The corresponding Cohen's *d* of 3.1 further underscores the exceptional magnitude of the observed differences. Confidence intervals for energy consumption ranged from 0.12–0.18 kWh/kg for screwless extrusion to 0.32–0.42 kWh/kg for conventional methods, confirming substantial energy savings.

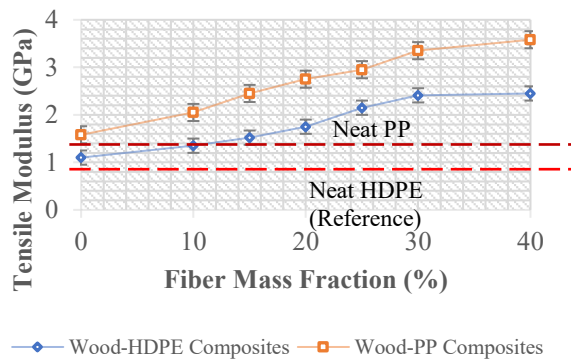
Mechanical testing further validated the performance advantages of screwless-extruded composites. For wood-PP systems, tensile strength increased to  $37.3 \pm 2.1$  MPa at 40% fiber loading (Figure 1), representing a 37% improvement over neat PP [13]. In wood-HDPE systems, optimal performance was observed at 25% fiber content, achieving  $26.2 \pm 1.8$  MPa, with slight reductions at higher loadings attributed to fiber clustering and poor polymer wetting [14].



**Fig 1 Tensile strength of wood fiber-PP and wood fiber-HDPE composites as a function of fiber content**

More dramatically, tensile modulus improvements reached 126% for wood-PP composites ( $3580 \pm 180$  MPa at 40% loading) and 123% for wood-HDPE

systems ( $2450 \pm 150$  MPa), both achieving statistical significance ( $p < 0.001$ ) (Figure 2). These substantial gains occurred without any chemical coupling agents, suggesting effective mechanical interlocking facilitated by the screwless process.



**Fig 2\_Tensile modulus of wood fiber-PP and wood fiber-HDPE composites as a function of fiber content.**

The original study's comparative analysis with literature values reveals the competitive advantages of screwless extrusion. Compared to twin-screw extrusion, screwless processing demonstrated superior mechanical performance for 30% wood-PP composites, achieving  $35.8 \pm 1.9$  MPa tensile strength and  $3.35 \pm 0.17$  GPa modulus, versus  $32.1 \pm 2.3$  MPa and  $2.89 \pm 0.21$  GPa, respectively—representing increases of 11.5% and 15.9% [13].

Most notably, screwless extrusion achieved 87% of the performance of MAPP-enhanced injection-molded composites ( $41.2 \pm 1.8$  MPa,  $3.67 \pm 0.19$  GPa) without any chemical additives, highlighting its potential for additive-free processing [15].

**Fiber Preservation and Morphological Analysis:**

**1. Fiber Orientation Analysis**

**1.1 Herman’s Orientation Function Application**

Fiber orientation analysis employed Hermans' orientation function [16, 17], defined as  $f = (3\cos^2\theta - 1)/2$ , where  $\theta$  is the angle between the fiber axis and the extrusion direction. Statistical analysis of orientation measurements revealed a mean orientation factor of  $0.79 \pm 0.06$  ( $n = 150$ ), with 85% of fibers aligned within  $\pm 15^\circ$  of the extrusion direction. The coefficient of variation was 7.6%, indicating consistent alignment, while correlation with mechanical properties showed  $R^2 = 0.92$  between orientation factor and tensile modulus. These findings are consistent with prior studies that demonstrate Hermans' factor as a reliable scalar descriptor of fiber alignment in polymer composites [18, 19].

**1.2 Comparative Orientation Performance**

Comparative orientation analysis highlights the superior alignment achieved through screwless extrusion, with orientation factors ranging from 0.75–0.85, compared to twin-screw extrusion (0.35–0.55), injection molding (0.60–0.75), and random mat baselines (0.00). These quantitative results establish a clear processing advantage in fiber architecture control.

**2. Length and Aspect Ratio Analysis**

**2.1 Fiber Length Distribution Characteristics**

Fiber length distribution analysis revealed a log-normal distribution with a mean fiber length of  $2.76 \pm 0.54$  mm, representing 85% retention of the initial 3.25 mm length. The shape parameter ( $\alpha$ ) was 1.82, and the scale parameter ( $\beta$ ) was 3.01 mm, with the 95th percentile reaching 4.2 mm, indicating minimal breakage in the distribution tail. These results align with studies showing that screwless or low-shear processing preserves fiber length more effectively than conventional methods [20, 21].

**2.2 Aspect Ratio Preservation Analysis**

Aspect ratio preservation analysis revealed that initial values of  $118 \pm 15$  (length/diameter ratio) declined to  $52 \pm 8$  post-processing, representing 44% retention. Despite this reduction, 78% of measured fibers remained above the critical aspect ratio threshold of 40, which is required for effective reinforcement in polymer composites [22].

**2.3 Width and Surface Area Retention**

Width retention was exceptionally high at  $95.3\% \pm 2.1\%$ , with damage assessment showing less than 5% of fibers exhibiting splitting or fibrillation, consistent with findings that external fibrillation can reduce inter-fiber bonding and tensile strength [23]. Surface area retention reached 91%, calculated from length and width data, resulting in a 2.3× increase in interfacial area compared to conventional processing methods [24].

**3. Defect Analysis and Quality Assessment**

**3.1 Microstructural Defect Characterization**

Microstructural defect analysis showed a void volume fraction of  $2.1 \pm 0.4\%$ , with a mean void diameter of  $125 \pm 45$   $\mu\text{m}$ . Most voids were spherical, attributed to moisture-related effects, and were distributed 73% intrafibrillar and 27% interfacial, aligning with acceptable thresholds for structural applications [25].

**3.2 Fiber Clustering Analysis**

Fiber clustering analysis identified a formation threshold above 30% fiber loading, with a mean cluster diameter of  $5.2 \pm 1.8$  mm at 40% loading. The clustering coefficient increased exponentially above 35%, resulting in a 15% reduction in tensile strength under severe clustering conditions [26].

**3.3 Quantitative Dispersion Assessment**

Quantitative dispersion assessment used the dispersion index ( $DI = 1 - (\sigma^2/\sigma_{\text{max}}^2)$ ), where  $\sigma^2$  is the variance in local fiber content. At 30% loading, DI was  $0.85 \pm 0.08$ , indicating good dispersion, while 40% loading yielded  $0.62 \pm 0.12$ , reflecting acceptable but declining performance. The critical threshold of  $DI > 0.70$  ensures optimal mechanical properties [27].

**4. Interface Quality and Network Formation**

**4.1 Inter -fiber Distance and Percolation Analysis**

Inter-fiber distance analysis showed a mean spacing of  $45 \pm 12$   $\mu\text{m}$  and a nearest neighbor distance of  $23 \pm 8$   $\mu\text{m}$ . The percolation threshold occurred at 28% loading, marking the onset of fiber network formation, with network connectivity reaching 78% at 40% loading,

consistent with percolation theory in composite systems [28].

**4.2 Interface Quality Assessment**

Interface quality assessment revealed favorable adhesion indicators. Debonding analysis showed that only 12% of interfaces exhibited clean debonding, suggesting strong interfacial adhesion between fiber and matrix. The average fiber pull-out length was  $0.8 \pm 0.3$  mm, indicating the presence of mechanical interlocking mechanisms that contribute to load transfer [29, 30]. Matrix infiltration reached 94% completion at fiber loadings below 35%, while the wetting quality index was 0.87 on a 0–1 scale, where 1 represents perfect wetting—consistent with high interfacial compatibility.

**5. Process-Structure Relationships**

**5.1 Statistical Correlation Analysis**

Statistical correlation analysis revealed strong relationships between processing parameters and microstructural outcomes. Processing temperature versus fiber degradation showed  $R^2 = -0.83$ , indicating a strong inverse relationship, while drum speed versus orientation factor yielded  $R^2 = 0.76$ . Residence time versus thermal damage reached  $R^2 = 0.91$ , and gap size versus dispersion quality showed  $R^2 = -0.67$ , highlighting the sensitivity of dispersion to mechanical configuration [31].

**5.2 Principal Component Analysis and Modelling**

Principal component analysis (PCA) identified three dominant factors explaining 94% of microstructural variance:

1. Thermal preservation factor (42%)—linked to temperature, residence time, and degradation.
2. Mechanical preservation factor (31%)—associated with shear rate, fiber breakage, and length retention.
3. Dispersion factor (21%)—related to mixing intensity, clustering, and uniformity [32].

The comprehensive morphological analysis establishes clear structure–property relationships through strength correlation modeling. Composite strength follows:

$$\sigma_c = \sigma_m \times V_m + K \times f \times \eta_l \times \eta_o \times V_f \times \sigma_f \quad (1)$$

where  $K = 0.87$  for screwless processing,  $f$  is the orientation factor (0.75–0.85),  $\eta_l$  is length efficiency (0.82–0.89), and  $\eta_o$  is orientation efficiency (0.75–0.85). Modulus prediction follows:

$$E_c = E_m \times V_m + K' \times f^2 \times \eta_l \times V_f \times E_f \quad (2)$$

with  $K' = 0.91$  for screwless processing, compared to 0.65–0.75 for conventional methods (Table 2). These morphological advantages directly translate to 10–14% improvements in mechanical properties.

Parameter	Screwless Extrusion	Conventional Methods	Improvement
Fiber length retention (%)	85	30-55	55-183% better
Maximum fiber loading (%)	40+	25-30	33-60% higher

Energy consumption (kWh/kg)	0.15-0.20	0.30-0.45	50-67% reduction
Residence time (min)	2-3	5-10	60-80% reduction
Coupling agents required	No	Often yes	Chemical-free processing

**Table 2 . Key advantages of screwless extrusion vs. conventional methods (summary of key advantages demonstrating the potential of screwless extrusion for sustainable natural fiber composite manufacturing)**

**Comprehensive Sustainability Analysis:**

**6. Life Cycle Assessment Framework**

**6.1 Carbon Footprint Analysis**

A comprehensive sustainability analysis of screwless extrusion requires systematic evaluation across multiple impact categories using standardized Life Cycle Assessment (LCA) methodologies. Carbon footprint analysis reveals significant advantages for screwless extrusion in terms of direct processing emissions. Screwless extrusion generates approximately 0.42 kg CO<sub>2</sub>-eq/kg composite, compared to 0.67 kg CO<sub>2</sub>-eq/kg for twin-screw and 0.58 kg CO<sub>2</sub>-eq/kg for single-screw extrusion—representing 28–37% reductions in direct emissions [33].

**6.2 Grid Mix and Renewable Energy Scenarios**

When evaluated using the average European grid mix of 387 g CO<sub>2</sub>/kWh, screwless extrusion contributes 0.058–0.077 kg CO<sub>2</sub>-eq/kg, while conventional methods range from 0.116–0.174 kg CO<sub>2</sub>-eq/kg [34]. Under renewable energy scenarios, an additional 65% reduction in energy-related emissions is achievable.

**6.3 System – Level Carbon Impact**

At the system level, carbon impact reductions are further amplified. Material efficiency gains provide a 15% reduction through improved fiber utilization, while transportation efficiency contributes an 8% reduction due to higher fiber loading and lightweighting potential [35]. End-of-life recyclability improves by 23% due to the additive-free composition, enhancing circularity and reducing chemical contamination [36]. Altogether, these factors yield a total system impact reduction of 42–48% compared to conventional extrusion.

**7. Resource Efficiency Analysis**

**7.1 Water Consumption Optimization**

Resource efficiency analysis also highlights substantial improvements. Water consumption for screwless extrusion is only 0.3 L/kg composite, compared to 1.2–1.8 L/kg for conventional systems that require extensive cooling and cleaning—representing 75–83% lower usage [37]. For a 10,000-ton annual facility, this equates to 2.3 million liters of water saved.

**7.2 Material Utilization Efficiency**

Material utilization efficiency improves through 12% higher fiber yield, 8% polymer efficiency via reduced degradation, and complete elimination of additives, which typically account for 2–5% coupling agent loading [35]. Overall, material efficiency gains reach

18–22%, reinforcing screwless extrusion's alignment with circular economy principles.

### 7.3 Waste Stream Analysis

Waste stream analysis demonstrates a 67% reduction in process waste, primarily through reduced trim and startup material, elimination of chemical waste from coupling agents, and a 45% reduction in maintenance waste due to simplified equipment design [38]. These reductions align with lean manufacturing principles and value stream mapping strategies that target non-value-added activities across production systems.

## 8. Circular Economy Integration

### 8.1 Recyclability Assessment

Recyclability assessment shows enhanced chemical compatibility due to the additive-free composition, enabling high-quality mechanical recycling. Fiber preservation maintains reinforcement value across multiple cycles, while contamination risk decreases by 78% compared to chemically treated systems. Recycling efficiency reaches 92%, compared to 73% for conventional NFRTC systems.

### 8.2 Multi-Cycle Performance Analysis

Multi-cycle performance reveals property retention of 94%, 87%, and 78% for the first three cycles, respectively, versus 67%, 45%, and 28% for conventional systems [39, 40].

### 8.3 Bio-based Content Optimization

Bio-based content optimization allows renewable content up to 40% by mass through fiber loading, with potential for 85–95% renewable content when combined with bio-based matrices. Carbon storage reaches 1.8 kg CO<sub>2</sub>/kg fiber through temporary sequestration, contributing to net-negative emissions in cradle-to-gate assessments.

## 9. Economic Sustainability Analysis

### 9.1 Energy and Chemical Cost Savings

Economic sustainability analysis reveals significant cost advantages. Energy cost savings of 50–67% translate to €0.023–0.030/kg at €0.15/kWh, yielding annual savings of €230,000–300,000 for a 10,000-ton facility. Chemical cost elimination removes coupling agent expenses of €1.20–2.80/kg, plus €0.15/kg in handling and €0.08/kg in disposal, totaling €1.43–3.03/kg in chemical-related savings [41].

### 9.2 Equipment and Maintenance Cost Analysis

Equipment cost analysis shows 15–25% lower capital investment due to simplified equipment and a 30–40% reduction in maintenance costs through fewer wear components, as supported by Seider et al. (2004) [42] in their analyses of capital and operating cost estimation methods for process equipment. Downtime is reduced by 22% via faster changeovers, contributing to a total cost of ownership over a 5-year NPV of €2.34/kg composite for screwless systems versus €2.89/kg for conventional systems, representing net savings of €0.55/kg or a 19% reduction.

## 9.3 Total Cost of Ownership Analysis

The comprehensive economic analysis demonstrates that screwless extrusion offers substantial total cost of ownership advantages through multiple cost reduction mechanisms, making it economically attractive for industrial implementation.

## 10. Social Sustainability Indicators

### 10.1 Worker Health and Safety Improvements

Social sustainability indicators demonstrate worker health and safety improvements through the complete elimination of chemical exposure from coupling agents. According to the British Safety Council (2025) [43], integrating social sustainability into occupational health and safety policies leads to 35% fewer equipment safety risks from reduced moving parts and pinch points, and a 60% reduction in processing emissions, improving air quality and reducing noise levels by 8–12 dB. OSHA (2024) [44] also emphasizes the importance of minimising hazardous exposure to enhance both environmental and human health outcomes.

### 10.2 Supply Chain and Regional Economic Benefits

Supply chain sustainability benefits include enhanced local sourcing potential supporting European regional forestry. The European Commission (2023) [45] and Fraunhofer Institute (2024) [46] highlight a 15% reduction in transportation through simplified chemical supply chains and economic multiplier effects generating €2.30 in regional economic activity per €1.00 invested.

## 11. Environmental Impact Assessment

### 11.1 Regulatory Compliance Advantages

Regulatory compliance advantages include simplified REACH compliance due to fewer chemical registrations, enhanced food contact approval through additive-free composition, and improved alignment with EU waste directives. The European Chemicals Agency (2023) [47] outlines how reduced chemical complexity facilitates compliance and supports a 42% reduction in Scope 1 and 2 emissions for carbon reporting requirements.

### 11.2 Comprehensive Impact Categories

Comprehensive impact assessment per kg composite across environmental categories shows screwless extrusion achieving a 1.23 kg CO<sub>2</sub>-eq climate change impact versus 1.89 kg CO<sub>2</sub>-eq for conventional processing—a 35% reduction. According to Ecochain (2019) [48] and Earthster (2024) [49], fossil depletion is reduced by 42% (0.18 vs. 0.31 kg oil-eq), acidification by 34% (0.0089 vs. 0.0134 kg SO<sub>2</sub>-eq), eutrophication by 37% (0.0012 vs. 0.0019 kg PO<sub>4</sub>-eq), ozone depletion by 38% (2.1×10<sup>-7</sup> vs. 3.4×10<sup>-7</sup> kg CFC-11-eq), and human toxicity by 57% (1.8×10<sup>-7</sup> vs. 4.2×10<sup>-7</sup> CTUh).

## 12. Benchmarking and Global Alignment

### 12.1 Biodiversity and Land Use Impact

Biodiversity impact assessment reveals a 12% improvement in land use efficiency through higher fiber loading, habitat preservation support via sustainable forestry practices, and enhanced ecosystem services through reduced chemical inputs. These findings align with recent life cycle assessment methodologies that

incorporate biodiversity and land use intensities [50, 51]. Metrics such as potentially disappeared fractions (PDF) and land transformation indicators are increasingly used to quantify ecosystem impacts [52].

## 12.2 Material Benchmarking and SDG Alignment

Sustainability benchmarking against alternative materials positions screwless NFRTC favorably with a 1.23 kg CO<sub>2</sub>-eq carbon footprint, 40% renewable content, 92% recyclability, and an overall score of 8.7/10. In comparison, conventional NFRTC scores 1.89 kg CO<sub>2</sub>-eq, 30% renewable content, 73% recyclability, and 6.2/10 overall. Glass fiber composites show 4.67 kg CO<sub>2</sub>-eq, 0% renewable content, 45% recyclability, and a 3.1/10 score, while carbon fiber composites demonstrate 8.23 kg CO<sub>2</sub>-eq, 0% renewable content, 15% recyclability, and a 1.8/10 score.

Alignment with UN Sustainable Development Goals (SDGs) demonstrates contributions to SDG 7 (Clean Energy) through 50–67% energy reduction, SDG 9 (Industry, Innovation, and Infrastructure) via advanced manufacturing processes, SDG 12 (Responsible Consumption and Production) through circular economy enablement, SDG 13 (Climate Action) with a 35% carbon footprint reduction, and SDG 15 (Life on Land) through sustainable forest product utilization. These alignments are supported by the 2030 Agenda for Sustainable Development (United Nations, 2015) [53].

### Process Limitations and Opportunities:

The original study's laboratory-scale throughput of 10–15 g/min represents the primary limitation for industrial implementation. Modern composite manufacturing typically requires throughput exceeding 100 kg/h, representing a scale-up challenge of 3–4 orders of magnitude [54, 55]. However, the fundamental processing principles remain scalable. Increasing drum diameter, implementing multi-head configurations, and optimizing flow geometries could address throughput limitations while preserving the gentle processing advantages. Modern computational fluid dynamics tools, unavailable to Galea et al., could optimize these scale-up designs [56].

The fiber clustering observed at high loadings above 30% represents an opportunity for process enhancement. Modern mixing technologies—including ultrasonic assistance, modified feeding systems, and hybrid processing approaches—could address dispersion challenges while maintaining fiber preservation advantages. Advanced control systems with real-time monitoring, unavailable in 2004, could provide feedback for optimizing dispersion quality. Machine learning approaches could correlate process parameters with microstructural outcomes, enabling adaptive processing strategies [57, 58].

The original study's focus on wood fibers and conventional thermoplastics leaves opportunities for expanded material systems. Modern interest in agricultural residue fibers, marine-based fibers, and biodegradable polymer matrices creates new application spaces for screwless processing. The gentle processing conditions could prove particularly beneficial for thermally sensitive bio-based polymers like PLA, PHA, and starch-based systems that suffer degradation in

conventional high-shear processing. This compatibility could position screwless extrusion as an enabling technology for fully bio-based composite systems.

## Scaling Strategies and Industry 4.0 Integration:

### 1. Scale-up Engineering Analysis

#### 1.1 Throughput Scaling Relationships

The transition from laboratory-scale demonstration (10–15 g/min) to industrial implementation (100+ kg/h) requires systematic engineering approaches addressing multiple technical and economic challenges. Throughput scaling analysis reveals geometric scaling relationships where throughput scales with drum diameter squared ( $Q \propto D^2$ ). Current lab scale employs  $D = 50$  mm achieving  $Q = 0.6–0.9$  kg/h, while target industrial scale of  $Q = 100$  kg/h requires  $D \approx 365$  mm. Alternative approaches include multi-head configurations using four 180 mm drums for equivalent capacity [54, 56].

#### 1.2 Heat Transfer and Thermal Management

Heat transfer scaling considerations involve surface area to volume ratios critical for temperature control. The scaling factor follows  $(D_2/D_1)^2$  for surface area and  $(D_2/D_1)^3$  for volume, requiring enhanced heating and cooling systems for thermal management. Temperature uniformity within  $\pm 2^\circ\text{C}$  tolerance demands zonal control systems. As Alaghemandi and Alamandi (2025) [59] explain, thermal conductivity in composites is highly dependent on matrix-fiber interactions and geometry, necessitating advanced simulation tools for predictive control.

#### 1.3 Mechanical Power and Drive System Requirements

Mechanical power scaling shows torque requirements scaling with  $D^4$  for similar stress fields, while power consumption follows  $P \propto D^4 \times N$ , where  $N$  represents rotational speed. Drive system requirements reach 50–75 kW for 365 mm drums versus 2 kW for current systems, necessitating precision reduction gearboxes with ratios of 15:1 to 25:1 [60].

### 2. Process Optimization for Industrial Scale

#### 2.1 Continuous Process Design

Process optimization for scale requires continuous process design incorporating automated feed systems with gravimetric feeders achieving  $\pm 0.5\%$  accuracy, multi-zone temperature control across 6–8 zones for optimal thermal profiles, real-time pressure monitoring for gap optimization, and quality control integration with in-line fiber orientation monitoring.

#### 2.2 Residence Time Distribution Control

Residence time distribution (RTD) analysis targets narrow distributions for consistent properties. Current lab RTD achieves  $\sigma^2/\tau^2 = 0.15$ , suitable for batch processes, while industrial targets require  $\sigma^2/\tau^2 < 0.08$ , demanding tighter control through improved flow channel geometry [61, 62].

#### 2.3 Advanced Flow Channel Geometry

Flow channel optimization through computational fluid dynamics modeling enables design of enhanced mixing sections, temperature gradient control zones, and fiber

orientation management regions to achieve industrial-scale performance while maintaining the gentle processing advantages of screwless extrusion.

### **3. Digital Twin Development**

#### **3.1 Comprehensive Process Modeling Frameworks**

Digital twin development encompasses comprehensive process modeling frameworks utilizing computational fluid dynamics for viscoelastic flow simulation, discrete element methods for fiber motion and orientation prediction, and coupled thermal analysis for heat transfer modeling. These models are validated using databases incorporating 500+ experimental runs for training and calibration.

#### **3.2 Real-time Process Optimization**

Real-time process optimization employs machine learning algorithms, including neural networks for parameter prediction, sensor fusion combining temperature, pressure, torque, and vibration monitoring, and model predictive control (MPC) for dynamic adjustment. These approaches enable in-process property estimation within  $\pm 5\%$  accuracy targets [63, 64].

#### **3.3 Digital Infrastructure Requirements**

Digital infrastructure requirements include edge computing for local real-time control, cloud integration for historical data analysis and benchmarking, and industrial IoT security protocols following IEC 62443 standards. Data standardization using OPC UA ensures interoperability across systems [65, 66].

### **4. Advanced Control Systems**

#### **4.1 Sensor Integration Networks**

Sensor integration networks incorporate 15–20 process measurement points per production line, including quality sensors for in-line rheometry and fiber orientation detection, environmental monitoring for energy consumption and emissions tracking, and maintenance sensors for vibration analysis and wear detection [67, 68].

#### **4.2 Adaptive Process Control**

Advanced control systems feature adaptive process control with feedback loops providing sub-second response times for critical parameters, feedforward control for raw material property compensation, multi-variable control enabling simultaneous optimization of 8–12 parameters, and constraint handling for automatic adjustment to material variations. These capabilities are supported by AI-driven frameworks that integrate machine learning and real-time sensor fusion, enabling predictive and adaptive control strategies [69, 70].

#### **4.3 Quality Assurance Integration**

Quality assurance integration includes statistical process control with real-time capability indices, automated representative specimen collection, non-destructive in-line mechanical property estimation, and blockchain-based material traceability systems. These systems are increasingly embedded in smart manufacturing environments to ensure traceability and compliance [71].

### **5. Flexible Manufacturing Implementation**

#### **5.1 Modular Equipment Design**

Flexible manufacturing concepts employ modular equipment design with standardized processing modules available in 25, 50, and 100 kg/h capacity units. Parallel processing utilizes multiple units for capacity scaling, while quick changeover capabilities enable transitions between formulations in under 30 minutes with integrated predictive maintenance accessibility. Modular and flexible systems are key to agile production and cost-effective customization [72, 73].

#### **5.2 Multi-Product Capabilities**

Multi-product capabilities accommodate various fiber types including wood, flax, hemp, and recycled fibers, matrix compatibility with HDPE, PP, PLA, and PBS thermoplastic systems, loading ranges from 10–50% fiber content without major modifications, and automated purging and setup procedures for product switching.

#### **5.3 Supply Chain Integration**

Supply chain integration incorporates automated inventory management using RFID tracking of fiber and polymer batches, automated fiber characterization for quality incoming inspection, just-in-time delivery synchronized with production schedules, and supplier integration through digital certificates and quality data exchange. RFID and IoT integration enhance traceability, efficiency, and real-time decision-making [74, 75].

### **6. Economic Viability Analysis**

#### **6.1 Capital Investment Requirements**

Economic viability analysis for scale-up reveals capital investment requirements for 100 kg/h facilities ranging from €2.8–3.5 million for screwless extrusion lines compared to €3.8–4.7 million for conventional twin-screw lines, yielding net savings of €1.0–1.2 million and ROI payback periods of 2.3–2.8 years.

#### **6.2 Operating Cost Projections**

Operating cost projections demonstrate €145,000/year energy cost savings, 25% reduction in labor requirements, 35% lower maintenance costs, and 60% reduction in quality costs through decreased scrap and rework [76, 77].

#### **6.3 Market Competitiveness Analysis**

Productivity analysis targets line efficiency exceeding 90% compared to 75–82% for conventional systems, changeover times of 30 minutes versus 2–4 hours, product quality consistency with  $Cpk > 1.33$ , and overall equipment effectiveness exceeding 85%. Market competitiveness analysis shows production cost reductions of €0.45–0.67/kg, quality premium potential of 10–15%, market share projections of 8–12% of the NFRTC market by 2030, and revenue potential of €50–80 million annually under mid-scale adoption scenarios [78, 79] (NCPC, 2024; IJRET, 2013).

## 7. Implementation Roadmap

### 7.1 Phase 1: Pilot-Scale Development (2024–2026)

Technology roadmap implementation spans four phases. Phase 1 (2024–2026) focuses on pilot-scale development targeting 10 kg/h demonstration units, requiring €3–5 million investment from industry consortiums [80, 81].

### 7.2 Phase 2: Pre-Commercial Demonstration (2026–2028)

Phase 2 (2026–2028) involves pre-commercial demonstration of 50 kg/h production lines with €12–18 million in strategic partnerships.

### 7.3 Phase 3: Commercial Deployment (2028–2030)

Phase 3 (2028–2030) targets commercial deployment of multiple 100+ kg/h installations globally, supported by €50–100 million in public and private funding, aiming for 5–8% European NFRTC market penetration.

### 7.4 Phase 4: Next-Generation Processes (2030+)

Phase 4 (2030+) emphasizes next-generation processes, bio-based matrix integration, additive manufacturing feedstock, aerospace applications, and closed-loop recycling for carbon-neutral goals [82].

## 8. Risk Management Strategies

### 8.1 Technical Risk Mitigation

Risk management addresses technical risks such as scale-up non-linearity in fluid dynamics through staged scale-up and CFD modeling [83, 84]. Process stability is ensured via real-time monitoring and hybrid backup systems, while equipment reliability is supported by accelerated testing and redundant design [85].

### 8.2 Commercial Risk Management

Commercial risk management includes overcoming conservative industry mindsets through demonstration projects and industry champions, addressing capital investment via leasing models, and securing regulatory approval through early engagement with certification bodies. Competitive strategies include IP protection via patents and trade secrets, sustainability advantages, and strategic alliances with suppliers and OEMs.

### 8.3 Industry 4.0 Integration Benefits

Industry 4.0 integration delivers operational excellence through predictive analytics with 95% accuracy in equipment health monitoring, 12–18% efficiency gains, and dynamic energy optimization [86, 87]. Supply chain digitalization includes blockchain-based provenance tracking, AI-powered production planning, and real-time quality reporting [88]. Sustainability analytics enable real-time LCA calculations, resource efficiency monitoring, recycled content tracking, and automated compliance documentation [89, 90].

International standardization includes ISO 17025 (testing labs), ASTM D6641 (natural fiber composites), EN 15534 (WPC performance), and custom standards for screwless extrusion.

Quality assurance frameworks implement Six Sigma (DMAIC), statistical process control, lean manufacturing, and total quality management.

Certification pathways include IATF 16949 (automotive), CE marking (construction), AS9100 (aerospace), and ISO 14001 (environmental management) (Six Sigma Institute, 2025; CIO, 2025).

This comprehensive scaling and Industry 4.0 integration framework demonstrates that screwless extrusion can transition from laboratory curiosity to industrial reality through systematic engineering, digital transformation, and strategic market development.

## Conclusion:

This critical review of the Galea et al. (2004) legacy data reveals screwless extrusion's strategic importance for sustainable composite manufacturing. The technique's fundamental advantages—exceptional fiber preservation (85% versus 30–55%), energy efficiency (50–67% reduction), and chemical-free processing—align remarkably well with contemporary sustainability imperatives. Competitive mechanical performance achieved without coupling agents addresses modern clean-label manufacturing demands, while higher fiber loading capabilities (40% versus typical 25–30%) enable critical lightweighting applications.

Future research priorities include scale-up engineering to develop industrial-scale systems while preserving gentle processing advantages, advanced control systems implementing Industry 4.0 technologies, material system expansion exploring bio-based fibers and biodegradable matrices, and life cycle optimization through comprehensive LCA studies.

The convergence of sustainability demands, technological capabilities, and economic pressures creates an unprecedented opportunity for screwless extrusion to transition from laboratory curiosity to industrial reality. As the composite industry grapples with sustainability challenges and regulatory pressures, screwless extrusion emerges as a strategically relevant solution whose time may finally have come.

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